

Weight Selection and Identification for \mathcal{H}_∞ Loop-shaping

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Introduction

Question Addressed

Given:

- Frequency response samples of the true plant
- Frequency domain closed loop specifications

Find: A model that approximates the plant in a suitable norm, such that
(behaviour of the plant in closed loop with *any* controller C which satisfies the given closed loop spec.s) \approx (behaviour of the model in closed loop with same controller)

\mathcal{H}_∞ Loop-shaping

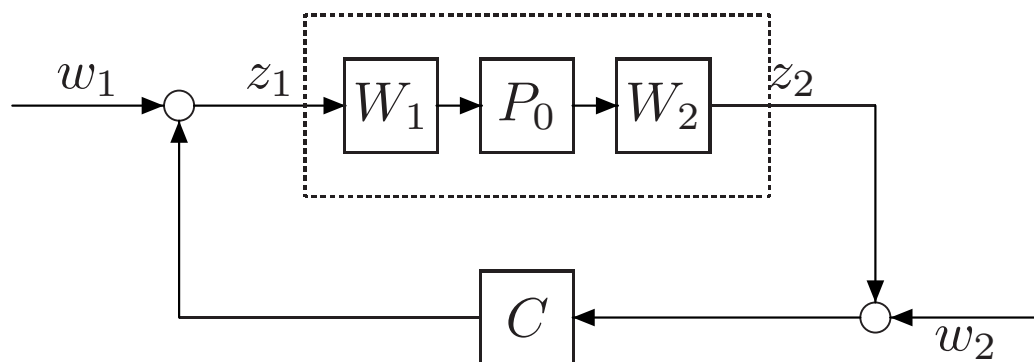
(McFarlane and Glover, 1990, 1992)

Define

$$\begin{aligned} H(P, C) & \text{ closed loop transfer function,} \\ & = \begin{bmatrix} P \\ I \end{bmatrix} (I - CP)^{-1} \begin{bmatrix} -C & I \end{bmatrix} \end{aligned}$$

$$\begin{aligned} b(P, C) & \text{ generalised robust stability margin,} \\ & = \|H(P, C)\|_\infty^{-1} \text{ if } H(P, C) \text{ is stable} \\ & = 0 \text{ otherwise.} \end{aligned}$$

$$\begin{aligned} \rho(P, C) & \text{ 'pointwise } b(P, C)\text{'}, \\ & = \frac{1}{\overline{\sigma}(H(P, C))} \end{aligned}$$



\mathcal{H}_∞ -Loop-shaping: Setup

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$$\begin{bmatrix} z_2 \\ z_1 \end{bmatrix} = H(P_s, C) \begin{bmatrix} w_2 \\ w_1 \end{bmatrix}$$

- W_1, W_2 are (usually) min. phase, diagonal transfer matrices such that $P_s = W_2 P_0 W_1$ has desired loopshape (*e.g.* large $\underline{\sigma}(P_s)$ in some low freq. region, small $\bar{\sigma}(P_s)$ in some high freq. region).

\mathcal{H}_∞ -Loop-shaping: Procedure

- Choose weights W_1, W_2 such that, for given loopshape bounds γ_1, γ_2 ,

$$\gamma_1(\omega) \leq \sigma_i(W_2 P_0 W_1)(j\omega) \leq \gamma_2(\omega)$$

holds for all ω .

- Solve

$$\sup_{C \text{ stabilising}} b(W_2 P_0 W_1, C)$$

(This has an analytic solution: McFarlane and Glover, 1990). Let C_∞ be the solution.

- Final controller is $C_s = W_1 C_\infty W_2$.

\mathcal{H}_∞ -Loop-shaping: Properties

- **Performance:** If the chosen loopshape ($\sigma_i(P_s)$) is compatible to robust stability requirement (*i.e.* if $b_{opt}(P_s)$ is large), $\sigma_i(P_0 C_s) \approx \sigma_i(P_s)$. W_1, W_2 are for performance; C_∞ - ideally - only adjusts phase for stability.
- **Robustness:** $b(P_s, C_\infty)$ represents robustness to normalised coprime factor perturbations; W_1, W_2 decide the shape of acceptable perturbations.

Question: If $b(P_s, C_\infty) > \beta$, what is the largest set of plants which is stabilised by C_∞ ?

The ν -gap metric

Define

G_i normalised right graph symbol for

$$P_i = N_i M_i^{-1} \quad (G_i = \begin{bmatrix} N_i \\ M_i \end{bmatrix} \text{ is inner })$$

$\eta(P)$ number of unstable poles of P

wno winding number; for $X, X^{-1} \in \mathcal{RL}_\infty$,

$$\text{wno det } (X) = \eta(X^{-1}) - \eta(X)$$

$I(P_0, P_1)$ wno det $(G_1^* G_0)$

The ν -gap metric: Definition

(Vinnicombe, 1993)

The ν -gap between two plants P_0 and P_1 may be defined by

$$\begin{aligned} \delta_\nu(P_0, P_1) &:= \inf_{\substack{Q, Q^{-1} \in \mathcal{L}_\infty \\ \text{wno det}(Q)=0}} \|G_0 - G_1 Q\|_\infty \\ &:= \sup_{\omega} \kappa(P_0, P_1)(j\omega) \text{ when} \\ &\quad I(P_0, P_1) = 0 \end{aligned}$$

The *pointwise chordal distance* $\kappa(P_0, P_1)$ defined by

$$\begin{aligned} \kappa(P_0, P_1)(j\omega) &:= \\ \bar{\sigma} \left((I + P_0 P_0^*)^{-\frac{1}{2}} (P_0 - P_1) (I + P_1^* P_1)^{-\frac{1}{2}} \right) (j\omega) \end{aligned}$$

The ν -gap metric: Properties

- For a plant P_0 , model P_1 and a controller C , at any point ω ,

$$\kappa(P_0, P_1) \leq \bar{\sigma}(H(P_0, C) - H(P_1, C)) \text{ and}$$

$$\bar{\sigma}(H(P_0, C) - H(P_1, C)) \leq \frac{\kappa(P_0, P_1)}{\rho(P_0, C) \rho(P_1, C)}$$

- Also,

$$\rho(P_0, C) \geq \rho(P_1, C) - \kappa(P_0, P_1) \text{ and}$$

$$b(P_0, C) \geq b(P_1, C) - \delta_\nu(P_0, P_1) \Leftarrow \text{tight bound}$$

- If P_1 is a model for plant P_0 ,
 - $\rho(P_1, C)$: designed performance.
 - $\rho(P_0, C)$: achieved performance.
 - $\kappa(P_0, P_1)$: difference in closed loop behaviour (**no C in this.**)

Weight Selection and Identification Problem

Given: Frequency response samples of plant P_0 , $P_0(j\omega_i)$, $i = 1, 2, \dots, m$ and loopshaping specifications $\gamma_{1,i}$, $\gamma_{2,i}$:

Find:

- Diagonal, stable min. phase t.f.s W_1, W_2 s.t.

$$\gamma_{1,i} \leq \sigma_i(W_2 P_0 W_1)(j\omega_i) \leq \gamma_{2,i}$$

- $\hat{P} \in \mathcal{S}$ for a suitable \mathcal{S} which solves

$$\min_{P \in \mathcal{S}} \max_i \kappa(W_2 P_0 W_1, P)(j\omega_i)$$

subject to a smoothness constraint on \hat{P}
and the constraint $I(W_2 P_0 W_1, \hat{P}) = 0$.

Weight Selection: Convex Feasibility Approach (Lanzon, 2000)

- Find diagonal, positive definite X_i, Y_i such that

$$\gamma_{1,i} X_i \leq P_0(j\omega_i)^* Y_i P_0(j\omega_i) \leq \gamma_{2,i} X_i$$

holds. Then

$$\gamma_{1,i} \leq \sigma_i(Y_i^{\frac{1}{2}} P_0(j\omega_i) X_i^{-\frac{1}{2}}) \leq \gamma_{2,i}$$

- Find minimum phase W_1, W_2 s.t.
 $W_1^{-*} W_1^{-1}(j\omega_i) \approx X_i, W_2^* W_2(j\omega_i) \approx Y_i.$
- It is possible to include further, useful convex constraints, *e.g.* bounds on condition numbers of X_i, Y_i .

Identification Problem

Given: Frequency response samples of shaped plant $P_s = W_2 P_0 W_1$,

$$P_s(j\omega_i), i = 1, 2, \dots, m$$

Find $P_1 \in \mathcal{S}$ such that

$$\begin{aligned} \inf_{Q, Q^{-1} \in \mathcal{L}_\infty} \max_i \bar{\sigma}(G_s - G_1 Q)(j\omega_i) \\ = \max_i \kappa(P_s, P_1)(j\omega_i) \end{aligned}$$

is minimised; subject to a smoothness constraint on P_1 and $I(P_s, P_1) = 0$.

Strategy for an approximate solution

(Date-Vinnicombe 1999,2001)

- Formulate an equivalent problem, in terms of $P_s(j\omega_i)$ instead of $G_s(j\omega_i)$;
- Choose a parameterised model set \mathcal{S} , solve

$$\min_{P \in \mathcal{S}} \max_i \kappa(P_s, P)(j\omega_i)$$

subject to some smoothness constraint on P . Let P_1 be the solution.

- Given a model P_1 and a controller C s.t. $\eta(H(P_s, C)) = 0$, find another model P_2 which satisfies $I(P_s, P_2) = 0$ and minimises $\max_{\omega} \kappa(P_1, P_2)$. Then

$$\max_i \kappa(P_s, P_2) \leq \max_i \kappa(P_s, P_1) + \max_{\omega} \kappa(P_1, P_2)$$

An Equivalent Problem Formulation

Lemma 1 *Given $P_s, P_1 \in \mathcal{RL}_\infty$, $Q, Q^{-1} \in \mathcal{L}_\infty$, $\exists \hat{Q}, F$ such that $\hat{Q}, \hat{Q}^{-1}, F \in \mathcal{L}_\infty$,*

$$\bar{\sigma}(G_s - G_1 Q)(j\omega) = \bar{\sigma}(F - G_1 \hat{Q})(j\omega) \forall \omega$$

and at any ω , complex matrix $F(j\omega)$ can be written as a function of point frequency response matrix $P_s(j\omega)$.

For a SISO system, we can choose F such that

$$F(j\omega_i) = \left[\frac{P_s(j\omega_i)}{\sqrt{1 + |P_s(j\omega_i)|^2}} \quad \frac{1}{\sqrt{1 + |P_s(j\omega_i)|^2}} \right]^T$$

Choice of Model Set (SISO case)

Let $S_n = \text{span} \{1, x, \dots, x^{n-1}\}$ where x is a fixed, first order transfer function. Let

$$S_{1,2} = \{f : f = [f_1 \ f_2]^T, f_1 \in S_{n_1}, f_2 \in S_{n_2}\}$$

For $f \in S_{1,2}$, the constraints

$$\max_i \bar{\sigma}(G_s - fQ)(j\omega_i) < \lambda \text{ and}$$

$\|f'\|_\infty < \lambda$ are affine in the parameters of f .

Chordal Distance Minimisation

Initialisation: Set $k = 1$, $\hat{Q}_0 = 1$.

Step A: Solve LMI optimisation

$$\min_{f_k \in \mathcal{S}_{1,2}} \max_{i \in [1, m]} \left\{ \bar{\sigma}(F(j\omega_i) - f_k(j\omega_i)\hat{Q}_{k-1}(j\omega_i)), \right. \\ \left. \alpha \|f'_k\|_\infty \right\}$$

where α is a user specified weight; $F(j\omega_i)$ derived from $P_s(j\omega_i)$. Let \hat{f}_k be the solution.

Step B: Solve

$$\min_{Q_k(j\omega_i)} \max_{i \in [1, m]} \bar{\sigma}(F(j\omega_i) - \hat{f}_k(j\omega_i)Q_k(j\omega_i))$$

Let $\hat{Q}_k(j\omega_i)$ be the solution. If $\max_i \bar{\sigma}(F(j\omega_i) - \hat{f}_k(j\omega_i)\hat{Q}_k(j\omega_i))$ is less than a specified tolerance, stop; otherwise set $k := k + 1$ and go back to step A.

For $\hat{f}_k = [\hat{f}_1 \hat{f}_2]^T$, the model obtained is $P_1 = \hat{f}_1 \hat{f}_2^{-1}$.

Winding Number Adjustment - 1

Idea (*Vinnicombe, 1993*):

Given P_1, P_2, C satisfying

$$\kappa(P_1, P_2)(j\omega)\bar{\sigma}(H(P_1, C))(j\omega) < 1 \forall \omega,$$

$$\eta(H(P_2, C)) = \eta(H(P_1, C)) + I(P_2, P_1)$$

\Rightarrow Given a controller C which stabilises shaped plant P_s and a model P_1 such that

$$\eta(H(P_1, C)) = k$$

find another model P_2 such that

$$I(P_2, P_1) \leq -k$$

$$\Downarrow \text{ if } \kappa(P_1, P_2)(j\omega)\bar{\sigma}(H(P_1, C))(j\omega) < 1 \forall \omega$$

$$\eta(H(P_2, C)) = 0$$

$$\Downarrow \text{ if } \kappa(P_2, P_0)(j\omega)\bar{\sigma}(H(P_2, C))(j\omega) < 1 \forall \omega$$

$$I(P_2, P_s) = 0 \quad (\text{since } \eta(H(P_s, C)) = 0)$$

Winding Number Adjustment - 2

Solution: Given P_1 , solution of the chordal distance approximation problem and a controller C that stabilises P_s , Solve

$$\inf_{\substack{P \in \mathcal{R} \\ I(P, P_1) \leq -k}} \sup_{\omega} \kappa(P_1, P)(j\omega)$$

where $k = \eta(H(P_1, C))$.

The solution to above problem may be characterised by solution of a Hankel norm approximation problem. If P_2 is a solution,

$$\max_i \kappa(P_s, P_2)(j\omega_i) \leq \max_i \kappa(P_s, P_1) + \max_{\omega} \kappa(P_1, P_2)$$

If $\eta(H(P_s, 0)) = \eta(H(P_1, 0)) = 0$, and $\max_i \kappa(P_s, P_1)(j\omega_i)$ is ‘small’, winding number adjustment is not required (i.e. P_1 is our final model.).

Weight and Model Re-adjustment

(Date-Lanzon, 2001)

Idea:

- Let \hat{P} be a model for plant P . For any compatible W_1, W_2 ,

$$\begin{aligned} & \rho(W_2PW_1, -(W_1^{-1}\hat{P}W_2^{-1})^\sim) \\ &= \sqrt{1 - \kappa^2(W_2PW_1, W_1^{-1}\hat{P}W_2^{-1})} \end{aligned}$$

- So

$$\min_{W_1, W_2} \kappa(W_2PW_1, W_1^{-1}\hat{P}W_2^{-1})$$

is equivalent to

$$\max_{W_1, W_2} \rho(W_2PW_2, -(W_1^{-1}\hat{P}W_2^{-1})^\sim)$$

Weight and Model Re-adjustment

Procedure:

- **Given:** $P_0(j\omega_i)$, model P_2 and weights $W_{1,0}, W_{2,0}$.
- Set $\bar{P} = -(W_{1,0}P_2^{\sim} W_{2,0})^{\sim}$.
- Solve, subject to constraints on $W_2P_0W_1$,

$$\max_{W_1, W_2} \rho(W_2P_0W_1, W_1^{-1}\bar{P}^{\sim}W_2^{-1})$$

This is convex in $W_1^{-*}W_1^{-1}$ and $W_2^*W_2$ (Lanzon, 2000).

- New weights: $W_{2,1}, W_{1,1}$, result of this optimisation.

New model: $P_3 = -(W_{2,1}^{-1}\bar{P}^{\sim}W_{2,1}^{-1})^{\sim}$.

$$\kappa(W_{2,1}P_0W_{1,1}, P_3) \leq \kappa(W_{2,0}P_0W_{1,0}, P_2)$$

Effect of Noise

Suppose, noisy freq. response samples,

$$P_{\omega_i} = P_0(j\omega_i) + v(j\omega_i), \quad i = 1, \dots, m$$

are given.

- Solve (approximately)

$$\min_{W_1, W_2, P} \max_i \kappa(W_2 P_{\omega_i} W_1, P)$$

Let $\hat{P}, \hat{W}_1, \hat{W}_2$ be the solutions.

- Then

$$\begin{aligned} \kappa(\hat{W}_2 P_0 \hat{W}_1, \hat{P}) &\leq \kappa(\hat{W}_2 P_0 \hat{W}_1, \hat{W}_2 P_{\omega_i} \hat{W}_1) \\ &\quad + \kappa(W_2 P_{\omega_i} W_1, \hat{P}) \end{aligned}$$

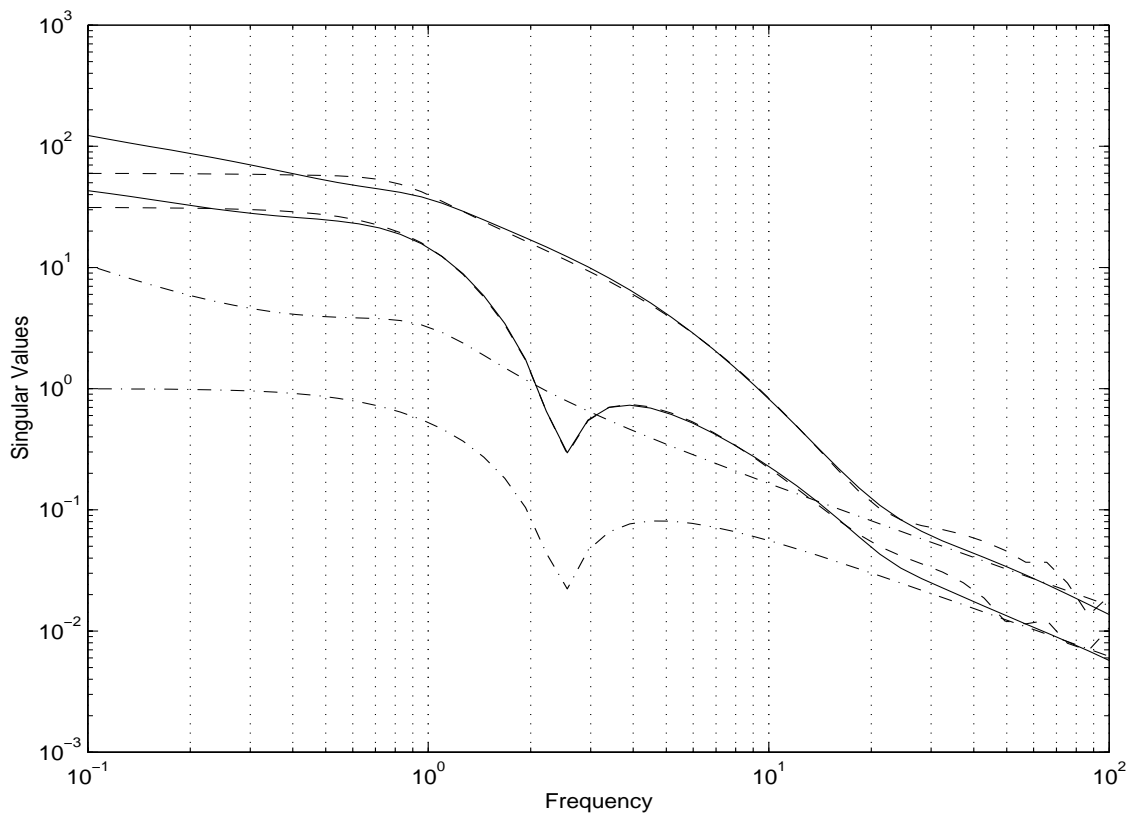
- First term is small if noise around closed loop crossover is small.

Simulation Example

$$\circ P_0(s) = \begin{bmatrix} \frac{1}{s+2} & \frac{1}{s} \\ \frac{1}{s-1} & \frac{3}{s^2+s+1} \end{bmatrix}$$

- 50 log-spaced freq. response samples betⁿ 0.1 rad/s and 100 rad/s .
- $\gamma_{1,i} \geq 25 \forall \omega_i \leq .5$.
- $\gamma_{2,i} \leq .1 \forall \omega_i \geq 20$.
- On solving feasibility problem and fitting transfer functions to pointwise weights: $W_1(s)$ of order 6, $W_2(s)$ of order 2.
- α chosen as .0010, model order = 18 ($n = 9$).

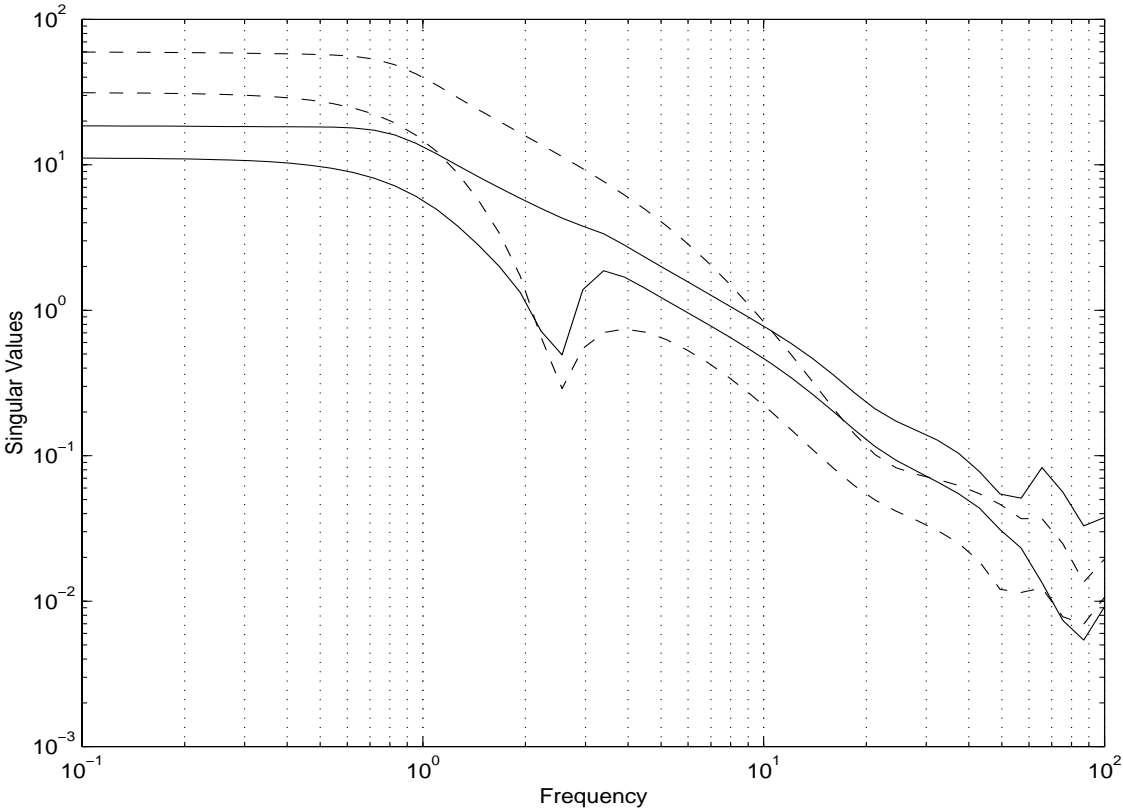
Singular Value Plots-1



(achieved $\max_i \kappa(W_2 P_0 W_1, P_2)(j\omega_i) = 0.0126$,
true $\delta_\nu(W_2 P_0 W_1, P_2) = 0.037$)

Singular Value Plots-2

Open and closed loop-shape for the model



Summary

- For a weighted plant $P_s = W_2 P_0 W_1$, model P_2 and a controller C , at any point ω ,

$$\rho(P_s, C) \geq \rho(P_2, C) - \kappa(P_s, P_2) \text{ and}$$

$$b(P_s, C) \geq b(P_2, C) - \delta_\nu(P_s, P_2)$$

- Weights W_1, W_2 can be obtained for given specifications using solution of convex feasibility problem.
- If chosen loop-shape is sensible and $\delta_\nu(P_s, P_2)$ is small, $b_{opt}(P_2)$ is large.
- $\max_i \kappa(P_s, P)$ explicitly minimised using a three step identification algorithm.
- Given P_2 , it is possible to re-adjust weights W_1, W_2 and model P_2 to reduce $\max_i \kappa(W_2 P_0 W_1, P)(j\omega_i)$ further.

Related Work

1. Date, Vinnicombe 2002: Given a bounded power excitation r , characterise the difference in the response of the designed and the achieved closed-loop to excitation r for ‘any’ controller.

2. Steele, Vinnicombe 2001: Given \hat{P} , $\{y_N, u_N\}$, ϵ , δ ,

$$\mathcal{P} = \{P : \underbrace{\|y_N - Pu_N\|_q}_{\leq \delta}, \delta_\nu(P, \hat{P}) \leq \epsilon\}$$

(something similar)

Is \mathcal{P} non-empty?